

[illegible]

.....	1
.....	1
.....	2
.....	8
.....	8
.....	13
.....	14
.....	29
.....	53
.....	54
.....	61
.....	70
.....	93
.....	96
.....	103
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.....	131
.....	131

	1							1992	65
		2009	8	27					
					2009	8	27		
	2							1986	36
		2009	8	27					
					2009	8	27		
	3							2013	
4	2014	1	1						
	4							2008	6
	2021	4	29						
								2021	4
	29								
	5							2002	70
		2021	6	10					
								2021	9 1
	1						2003	393	2004 2
1									
	2						2006	466	2014
7	29			653					2014
7	29								
	3						2019	708	2019 4 1
	1								

	2015	13	2015	2	13		
2							
	2015	75	2015	7	1		
3							2006
3	2015	5	29			80	
							2015 7 1

2024 1 16

14

10	GB 50052-2009
11	GB50057-2010
12	(GB50057-2010[2016])
13	GB50057-2010
14	GB 50057-2011
15	GB 50057-2012
16	GB50187-2012
17	GB50029-2014
18	GB50201-2014
19	GB 51016-2014
20	2018 GB50016-2014
21	GB55037-2022
22	GB 18306-2015
23	GB50150-2016
24	< 1 GB 6722-2014/XG1-2016
25	GB/T13869-2017
26	GB/T10595-2017
27	
28	GB/T8196-2018
29	GB18218-2018
30	GB51119-2015
31	GB 2811-2019
32	GB/T 38304-2019
33	GB/T 38509-2020
	5
	GB/T 2893.5-2020
	GB50070-2020

37	4	GB 39800.4-2020
38	GB16423-2020	
39		GB/T29639-2020
40		GB/T12265-2021
41		GB/T12719-2021
42		GB/T 20645-2021
43		GB/T23821-2022
44		GB/T13861-2022
1.2.5.2		
1		AQ2005-2005
2	AQ8001-2007	
3	AQ8002-2007	
4	AQ1043-2007	
5		
AQ2027-2010		
6		AQ/T 2063-2018
7		
AQ/T2073-2019		
8		AQ/T 1009-2021
9		AQ/T 1118-2021
1		
	2020	10
2		
	2022	2
3		
	2023	6
4		

2023 10

5

2023 42

2023 12 27

6

2023 43

2023 12 26

7

2024 4

1

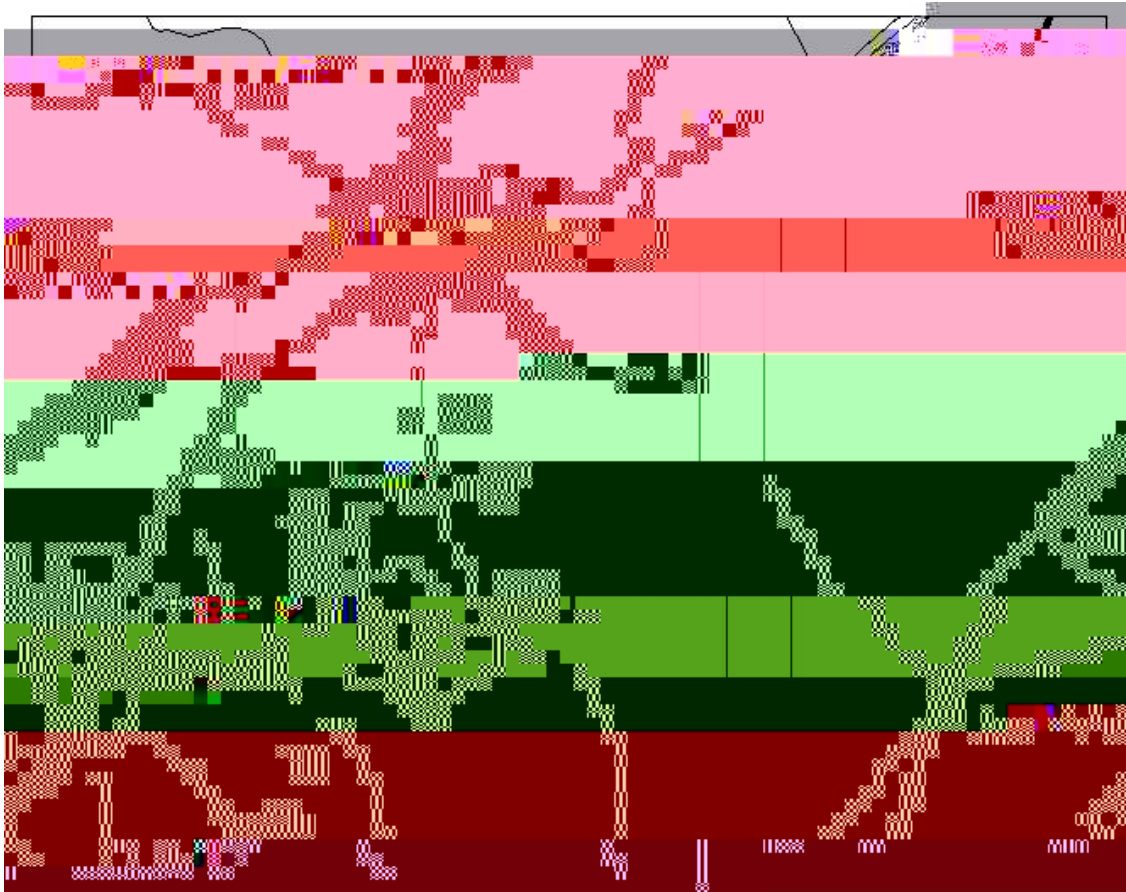
2

3

2-1

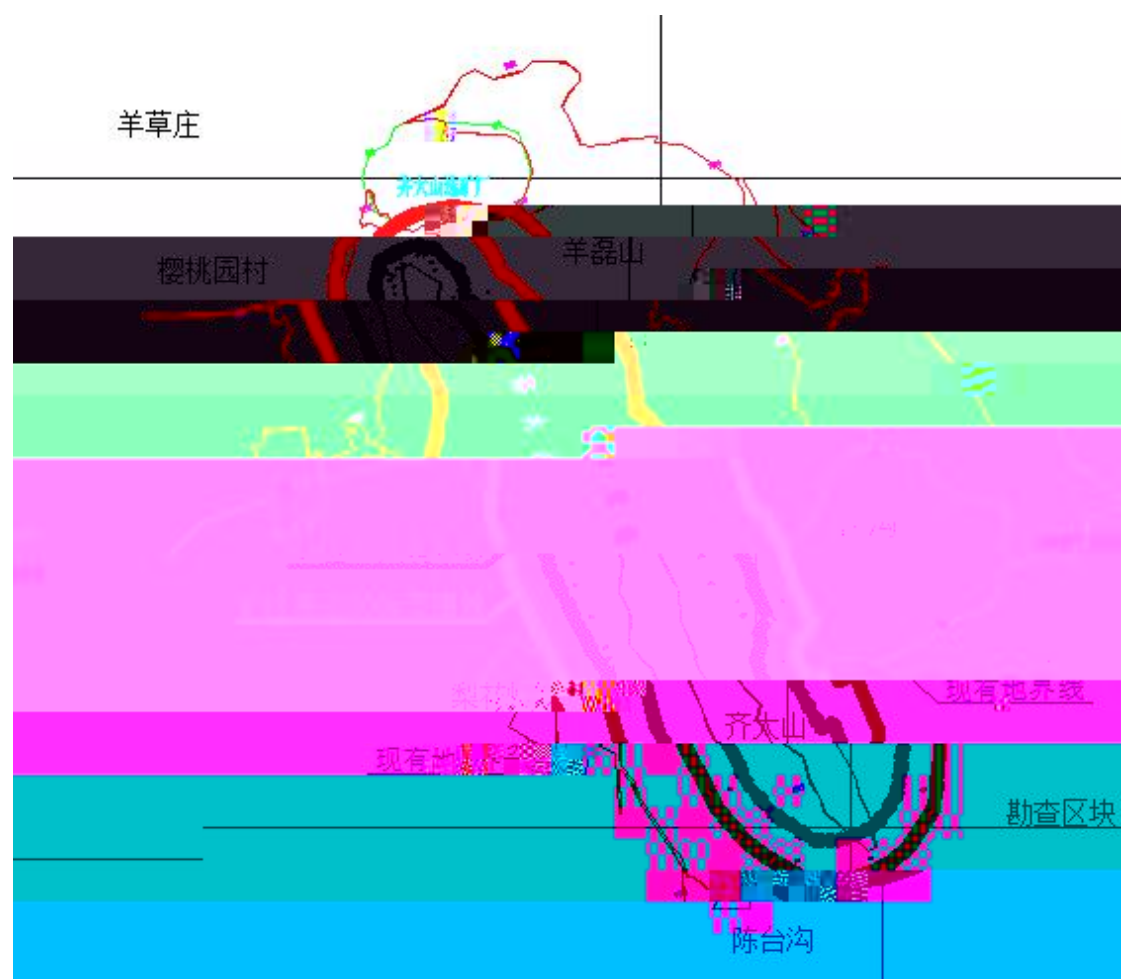
123 05 07

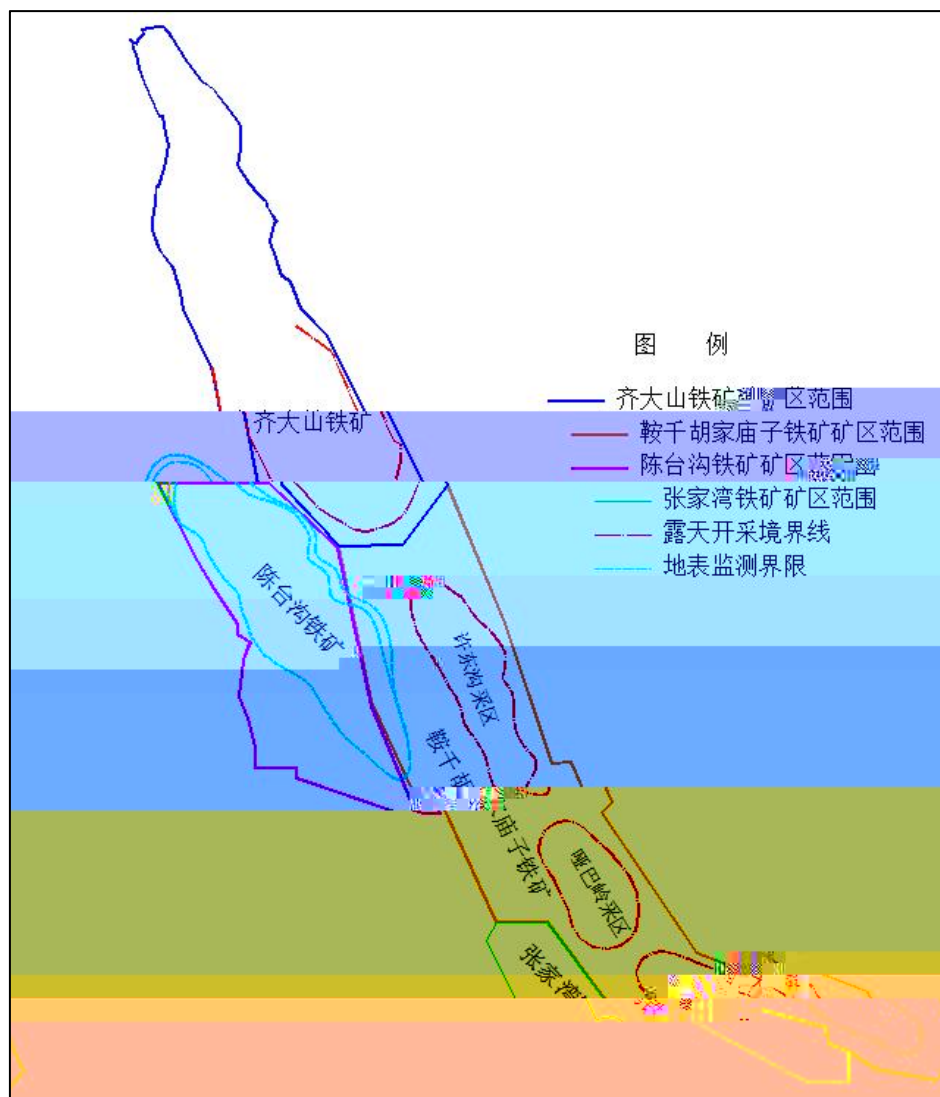
41 07 09



2







3

1 3m

50

2.3.1.2

1

		1480	3420m
310°	335°		86°

2-3

2.3.1.3

1

γ_1^2

1680

4500

-1200m

2

a. δ

b. μ

研究

1

4900 60

173 100 200m

3400m 1410m

133.72 -1385m 0m 1230m

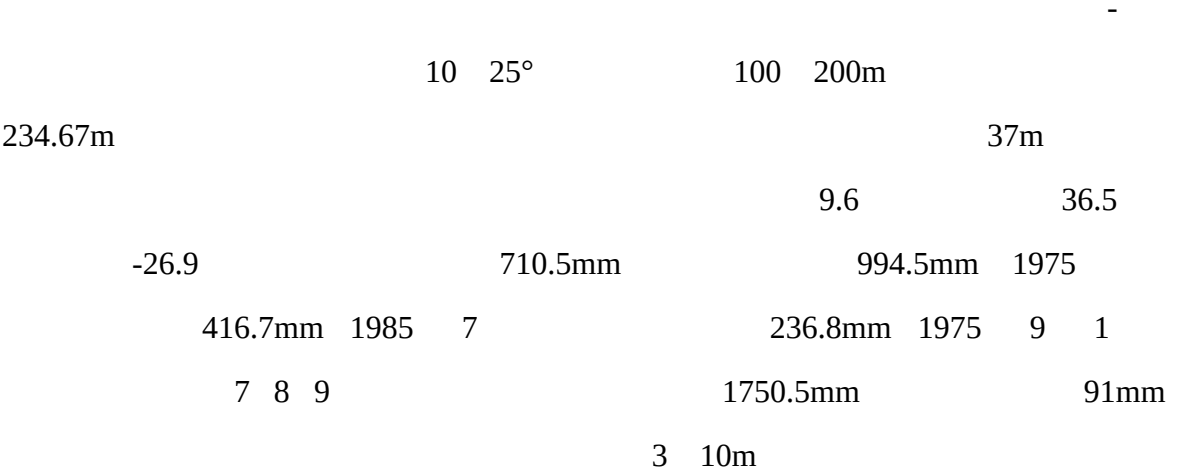
305 335° 70 90° TFe

31.20% 9.23% 36.3 267.5m 152.58m

42.92%

60 1060

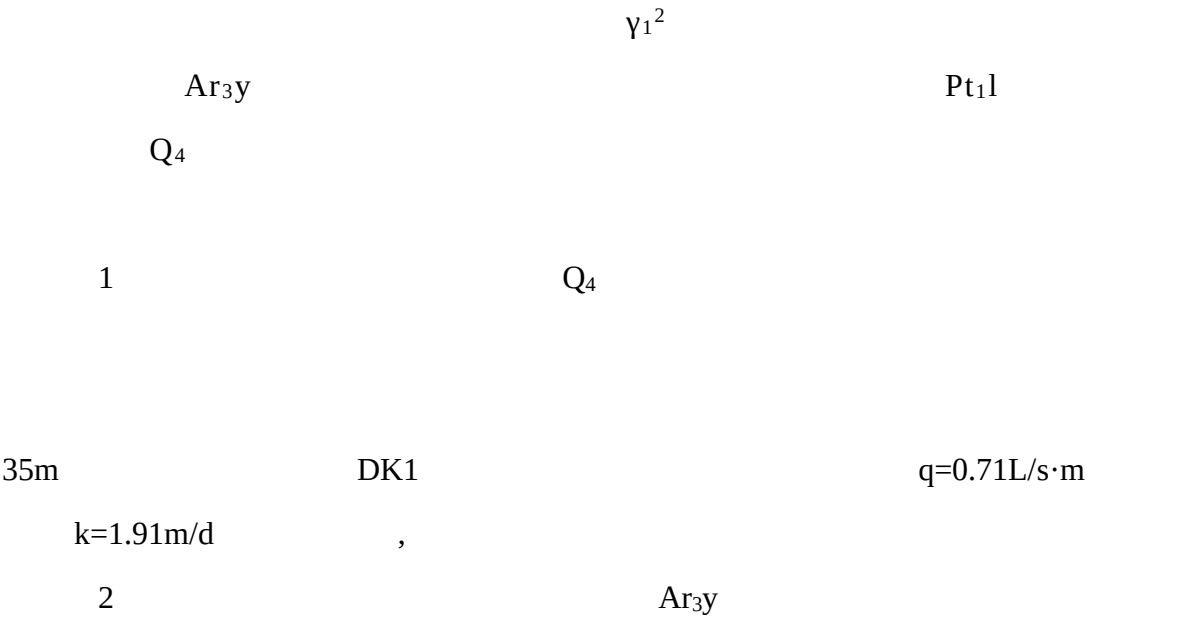
2.3.3.1



0.16m³/s

34.5m³/s

2.3.3.2



[illegible]

1

1-4m

1-2

1m

2-3

2

,

0.0006L/s·m

0.00027m/d

-48m

-69m

2.3.3.4

3P k

1260 1880

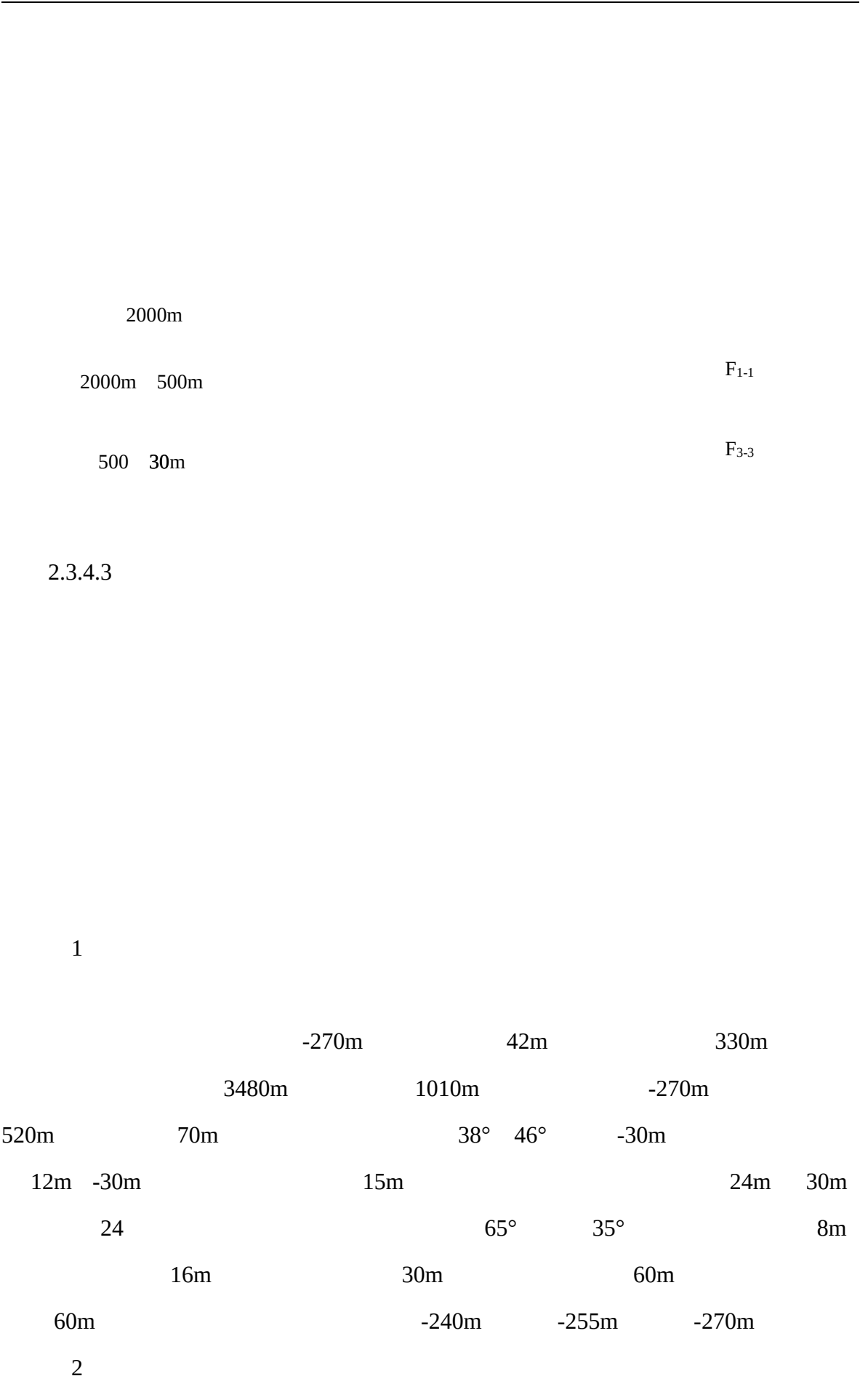
30m 50m

2cm 5cm

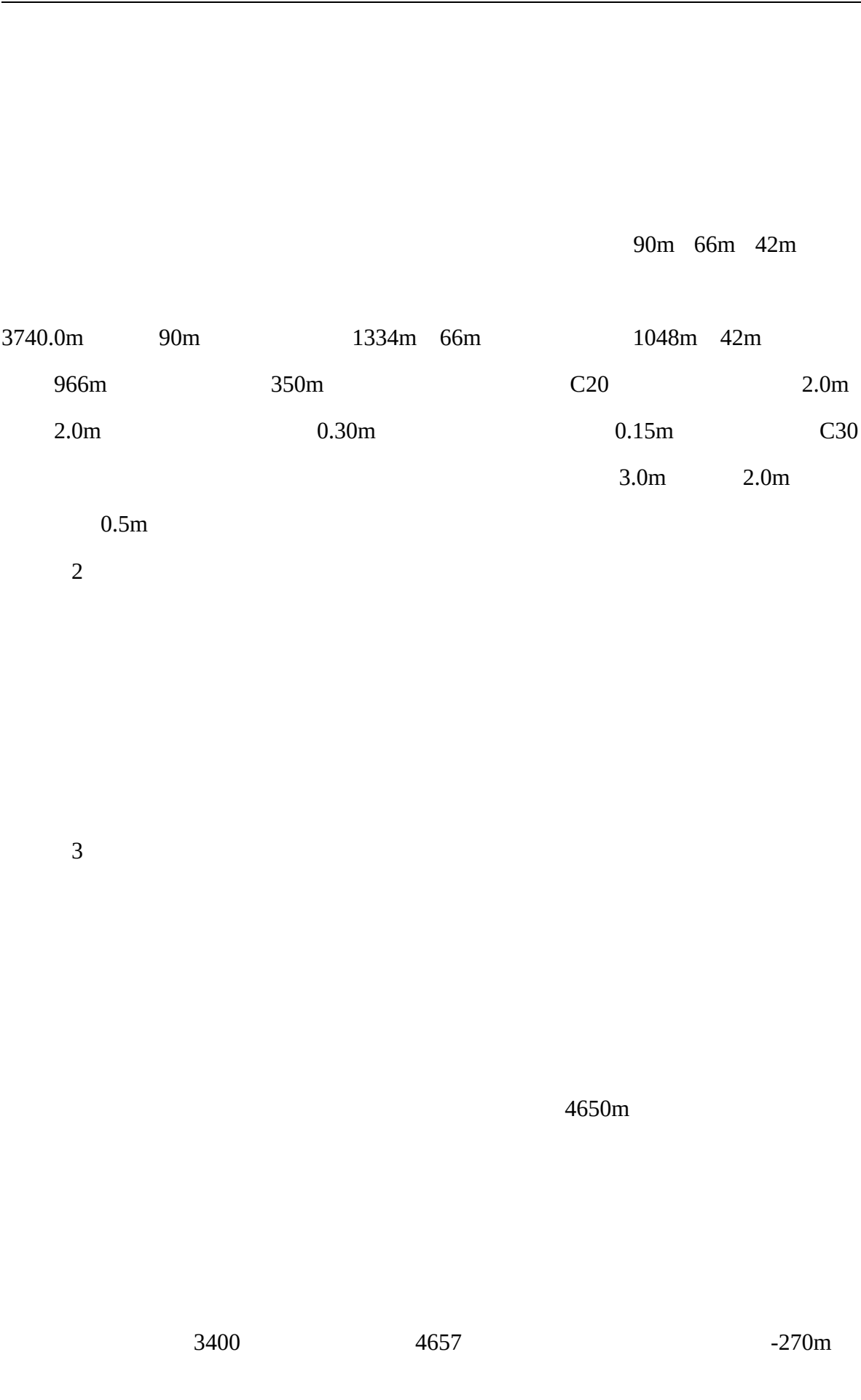
240 250°

32° 38°

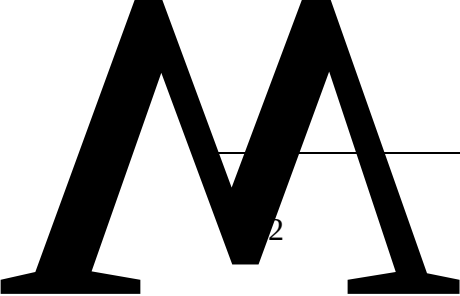
3



[illegible]



-450m



2

42m

-6m

50m

-330m

154 190t

30m

22m

1m

0.4m

0.4m

4m

2m

8%

60m

30m

1

2

5

3

2

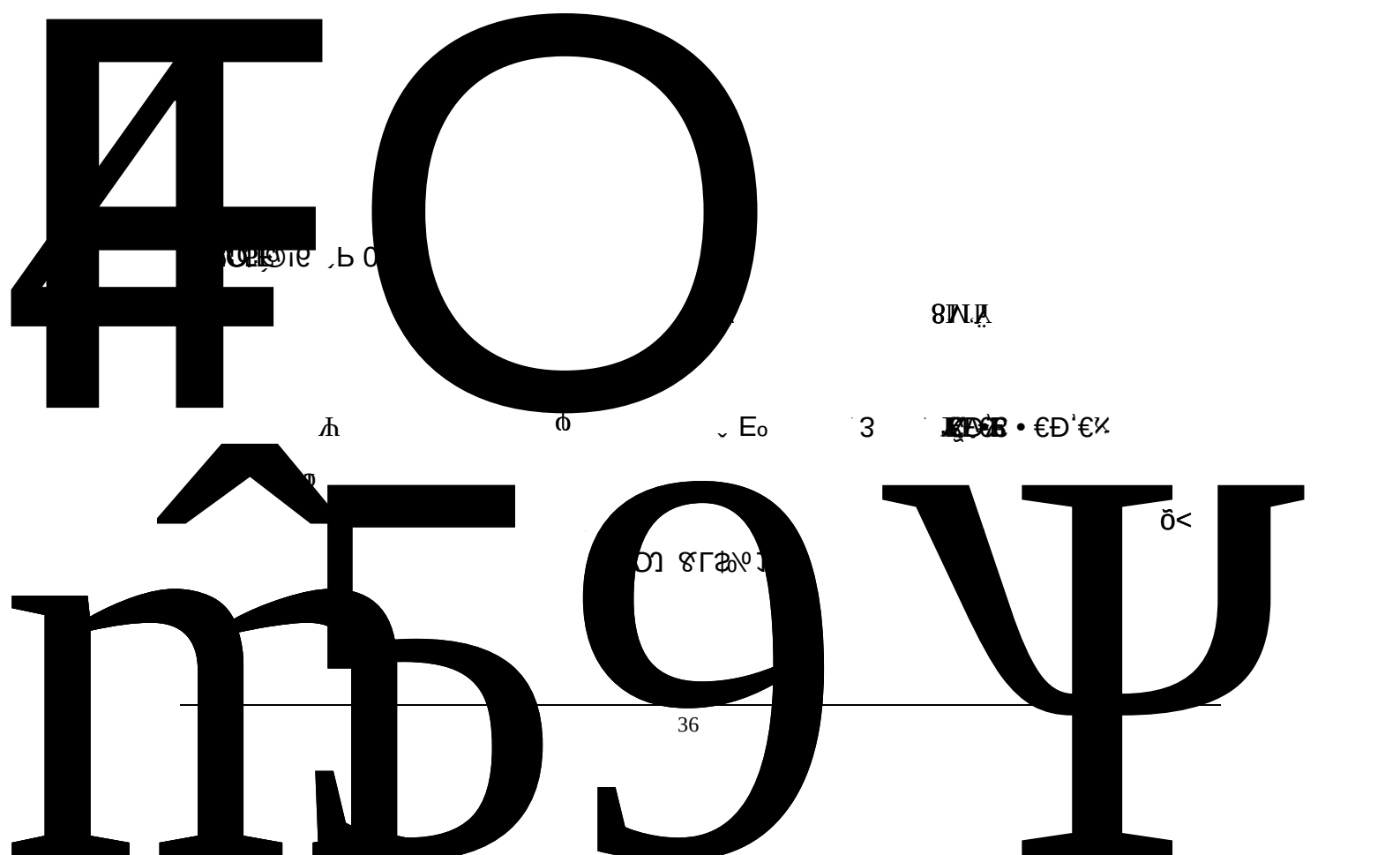
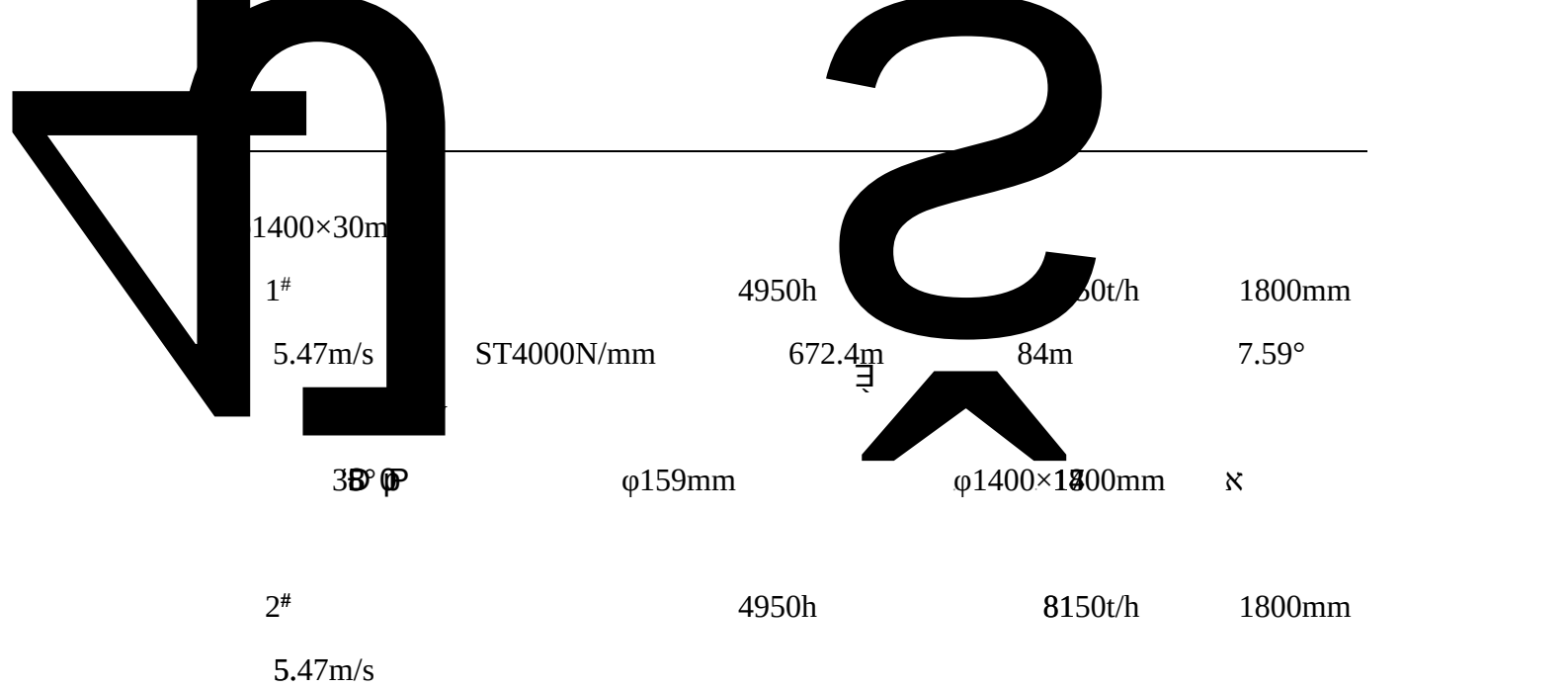
1

1997

-135m

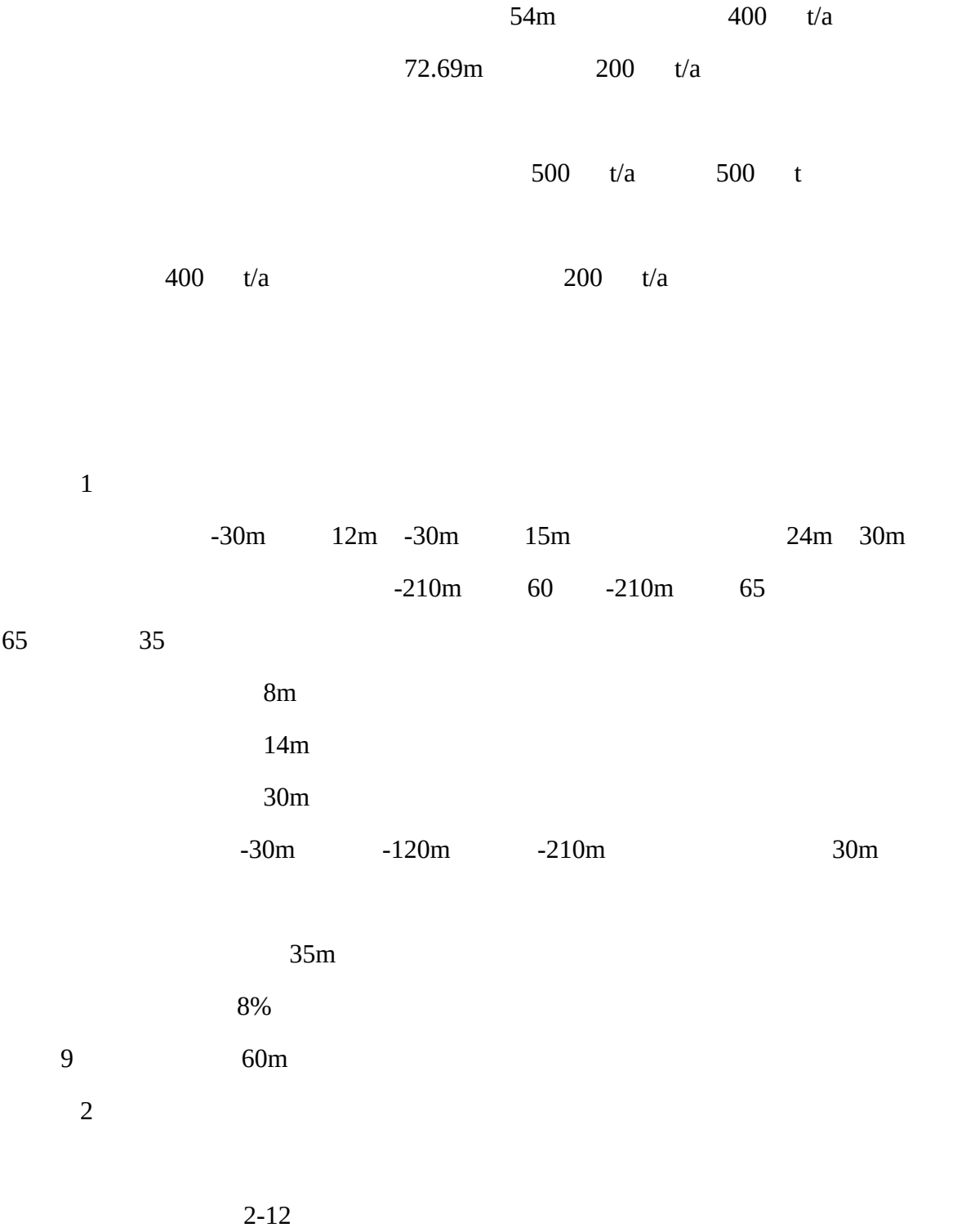
-108.5m

1700



				3 [#]	2 [#]
b					
1 [#]			1 [#]		4950h
1150t/h	1200mm	2.5m/s	ST1000N/mm		472.485m
28.3m	12.718°		400kW		
	35°		φ133mm		φ1000×1400mm
2 [#]				4950h	1150t/h
1200mm	2.5m/s	ST3150N/mm		693.523m	173.5m
14°		2×630kW			
35°		φ133mm		φ1400×1400mm	
3 [#]			4950h		1150t/h
2.5m/s	ST1000N/mm		178m	0m	0°
160kW					35°
φ133mm		φ1000×1400mm			
4					
					500 t/a
		→	→	→	1 [#] → 2 [#]
⊕					
	:500 t/a		330	3	8
	1000mm				
⊙					
a					
			+52.15m		





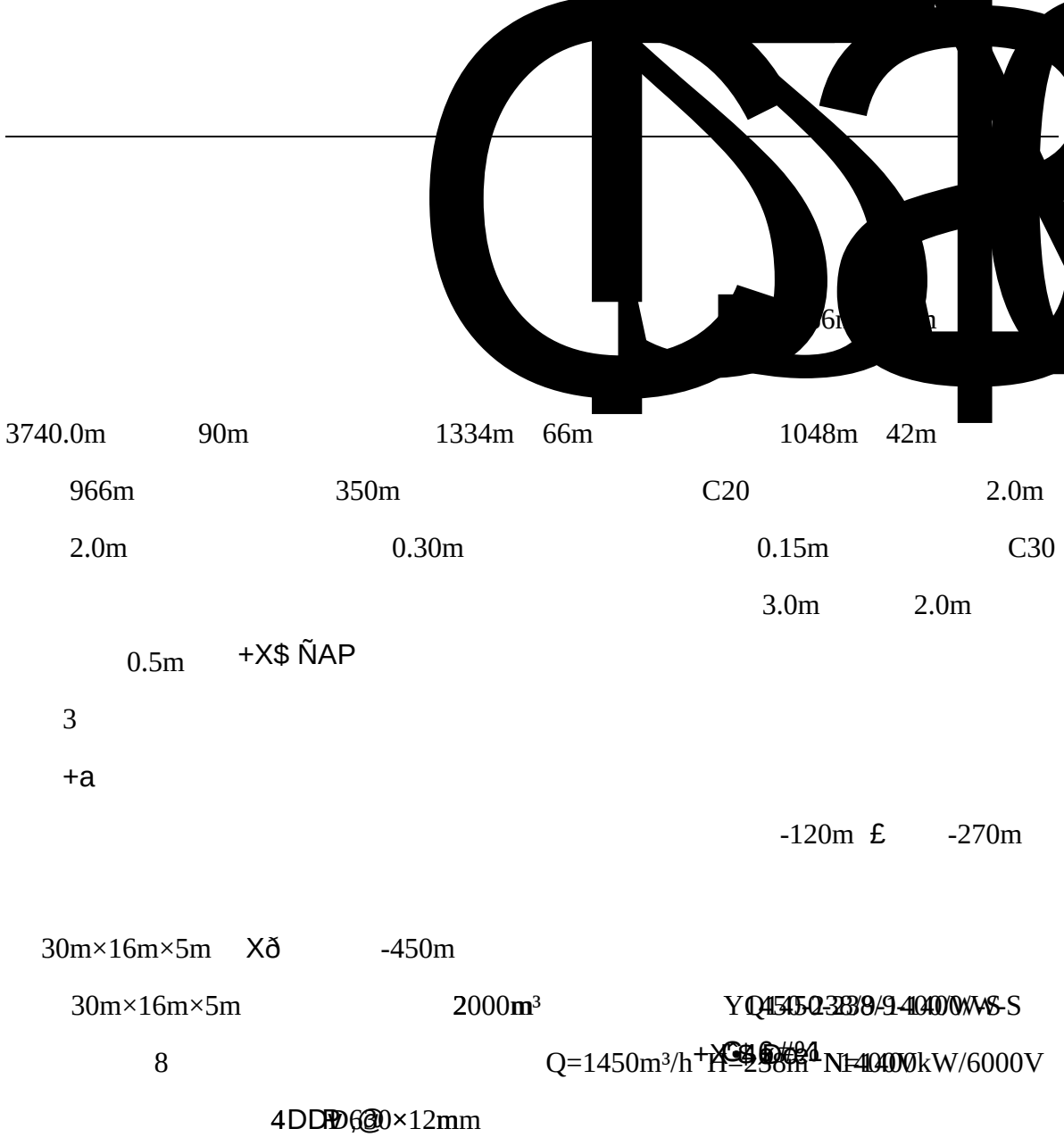
1			m	12	15	24	30
2				35			
				60			

						65			
						14.57			
						41.59			
3						44.68			
						41.98			
					m	8	8	14	
4					m	8	8	14	
5	-30	-120	-210		m	30			
6					m	30			
1					m	4849	1568	850	
2					m	2549	110	35	
3					m	-450			
4					m	596			
5					m	42			
					t	36704.88			
6					t	79682.45			

				250	310mm	14.5			
17.5m		2.5m	250mm			7m	6m	310mm	
8m	8m	550			t/	3%			110t/m
		7300	t/a						
			3	7	4			6	

			6	10kV		130 [#]	
		1 [#]	2		1 [#]		2 [#]
3 [#]	2		1 [#]		2 [#]	4 [#]	2
3							
-450m							

										PE	
1											
2.4.8.1											
1											
				-270m	6		1222m³/h				
185m		1000kW		3		φ426mm		3			
				-135m		1		9#			
7# 6# 5# 4# 2#				2							
4		2									
				2520m³/h							
2											
1											
79m		537m	2195m	2811m		4.0m					
6.0m	1		0.5				3.0m	2.0m			
0.5m		3		2.5m							
C30		C30									
2											



8369 m³

50m 20m 10m

2.4.9.3

78859 t 38084 m³
31729 m³ 6355 m³
8369 m³ 2-14

			m ³	
1		320	16176	
2		320	15553	
3		330	8369	
			40098	
			38084	
			2014	

2.4.9.4

850m 320m 16176 m³

1200m 320m 15553 m³

-

1

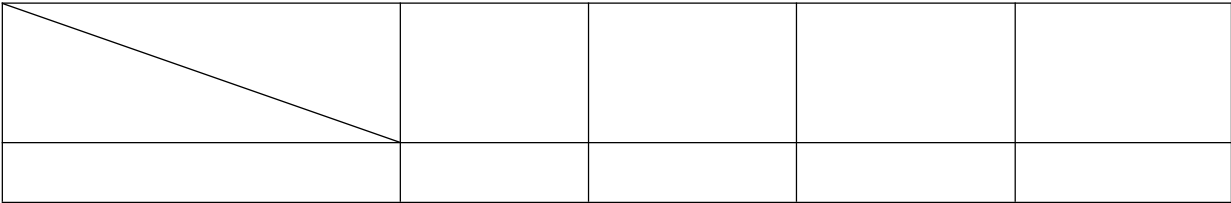
2

8

3

3-1

3-1

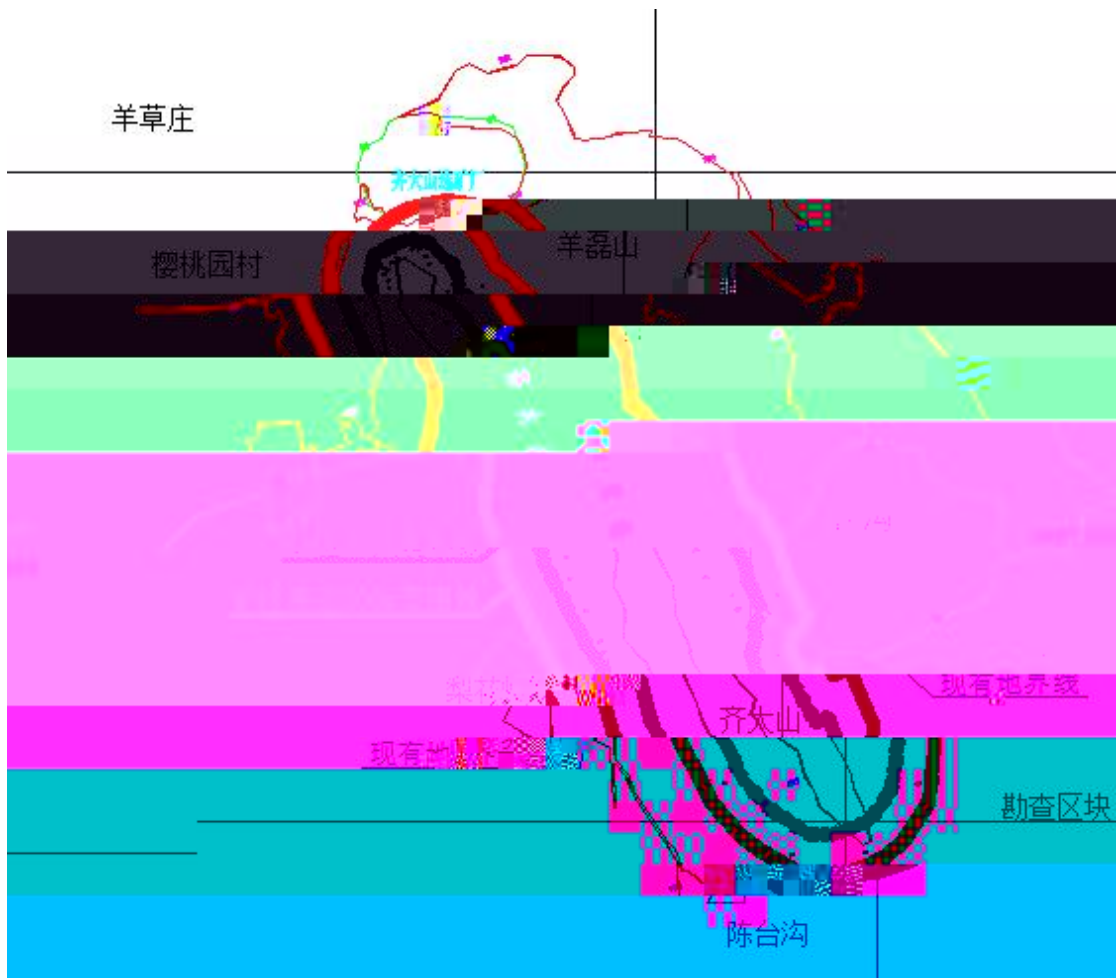
				

3.

3.0.10

4

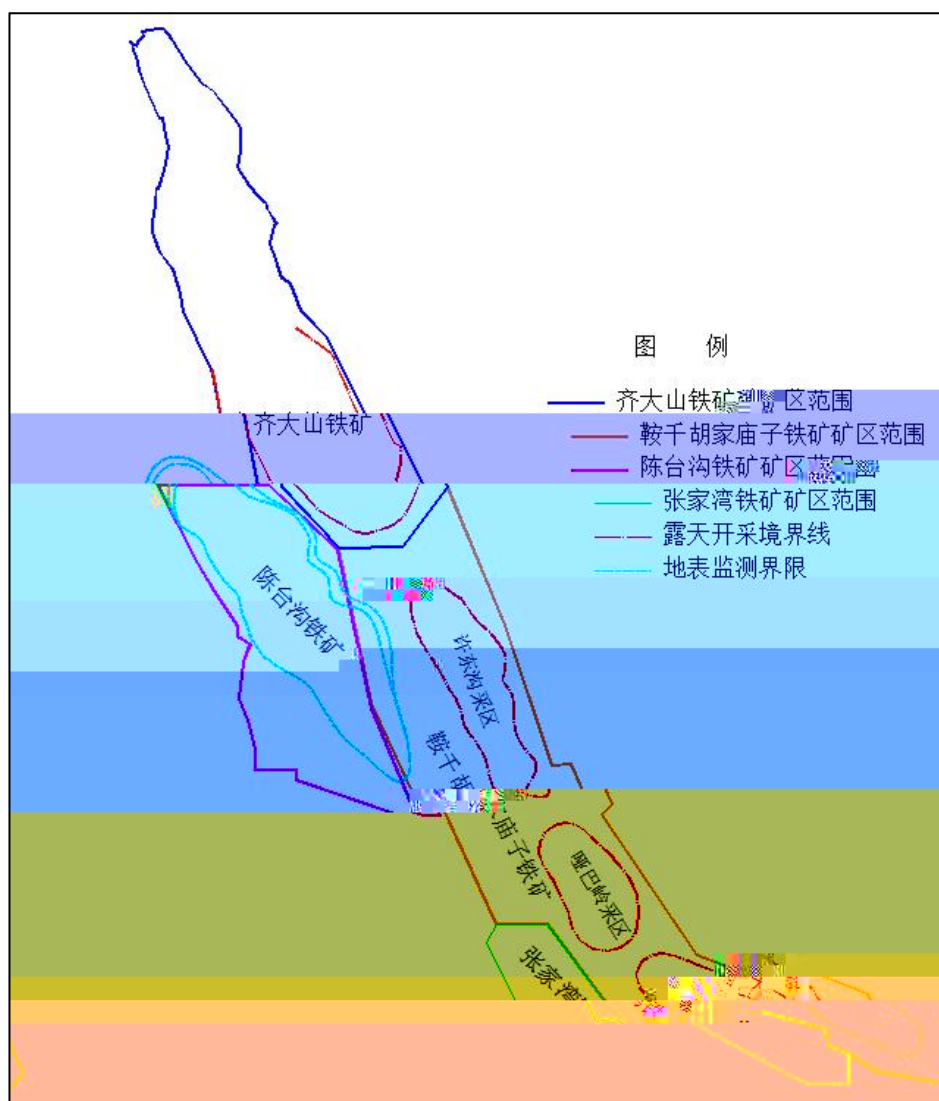
1



2

500m

30m



154 190t

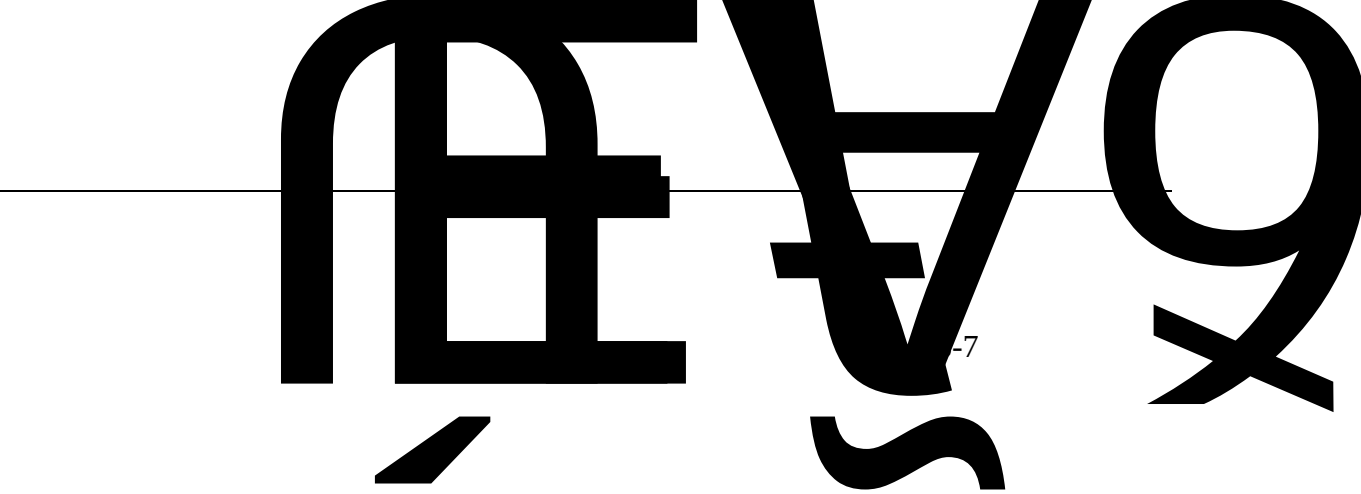
1

2

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5



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- 9.
- 10.
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- 2q
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^G ^{Y'} ^ī

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- 10.
- 11.
- 1.
- 2.
- 3.
- 1.
- 2.

1/2



“ ”

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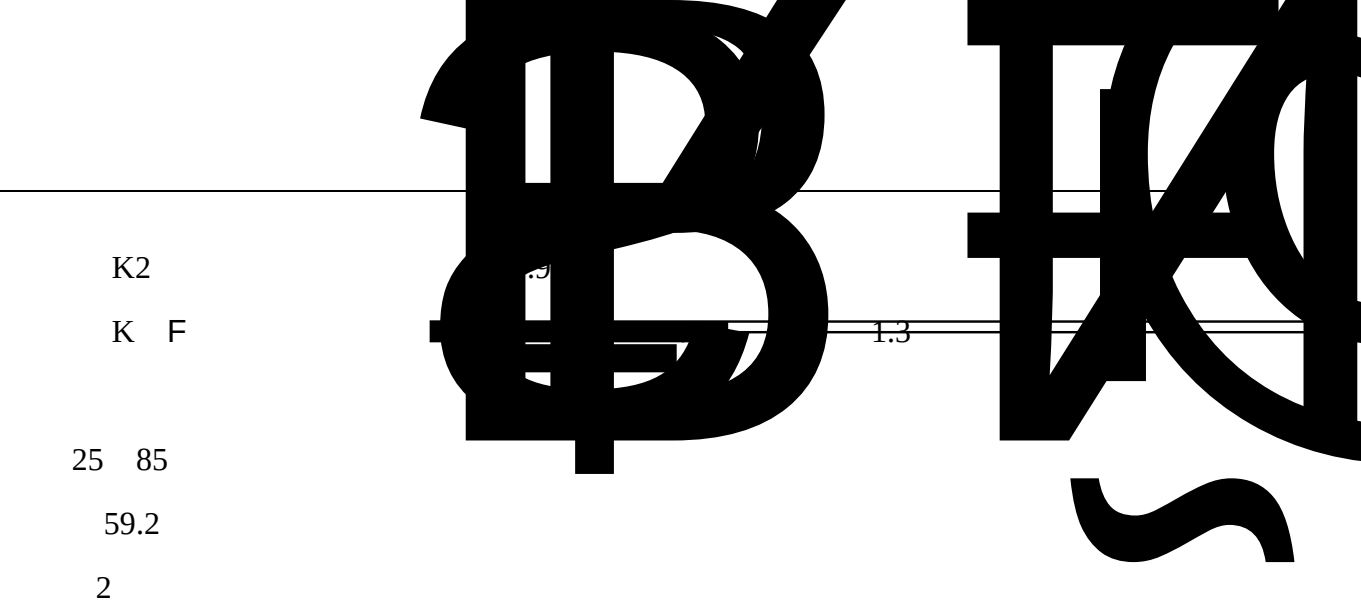
4.

5

6.
1.



3IK



			1. 2. 3. 4.		1. 2.
			1. 2. 3. 4. 5. 6. 7. 8. 9. 10.		1. 2. 3. 4. 5. 6. 7. 8. 9. 10.
			1. 2.		1. 2.
2			1. 2.		1. 2. 3.
			1. 2. 40		
3			1. 2.		1. 2.
			1. 2. 3.		
4			1. 2.		1. 2.

					3.
			1. 2.		
			1. 2.		1. 2.
5					
6			1. 2.		
7			1. 2. 30% 3. 10 20	10%	
8					

8

	Sf	Sd	S		
1	10			RPN= Sf×Sd×S	RPN
	Sf	Sd	S	5	
3-9					

	Sf	Sd	S	RPN		
	8	3	5	120	2	2
	4	3	4	48		

	4	4	4	16		
	7	4	6	168	1	1
	3	2	3	18		
	5	3	6	90	4	4
	4	4	6	96	3	3
	5	3	5	75	5	5
	3	5	3	45		

3-9

3

FMEA

3-10

	1.	GB18152-2000 7.1.1		
	—			
	—			
	—			
	2.	GB18152-2000 7.1.2		

3

GB18152-2000
7.1.3

4.

GB18152-2000
9.2.4

5.

GB18152-2000
9.2.8

6.

	8. 7 8 10	GB16423-2020 5.4.3.3		
	9. 3	GB16423-2020 5.4.3.4		
	10.	GB16423-2020 5.4.3.5		
	11.	GB16423-2020 5.4.3.6		

12.

1.0m

1.0m
0.6m

3.3.1.2

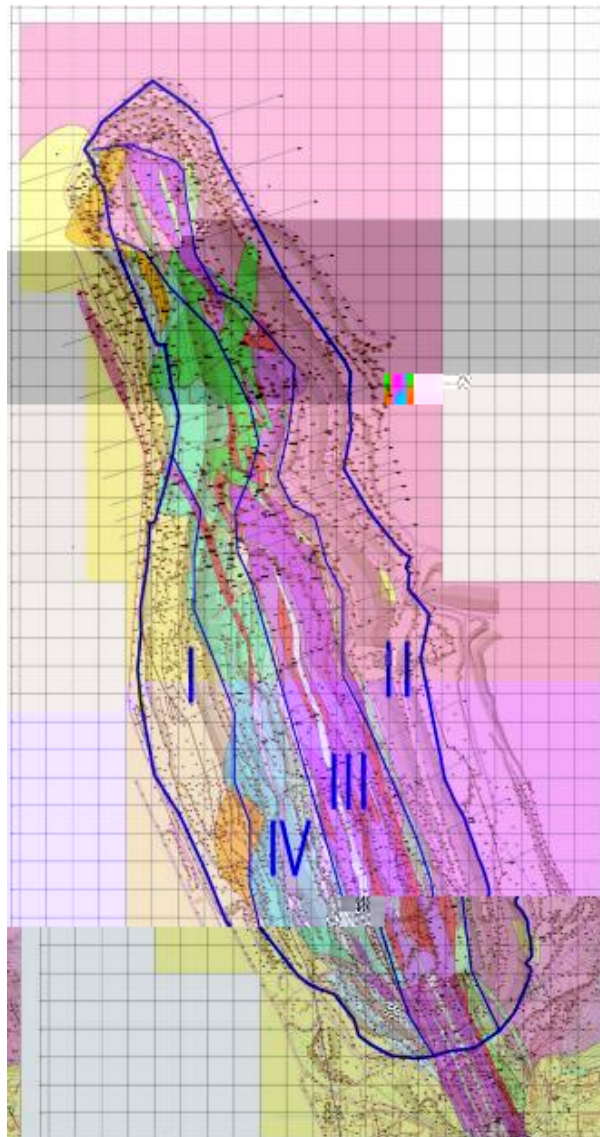
1

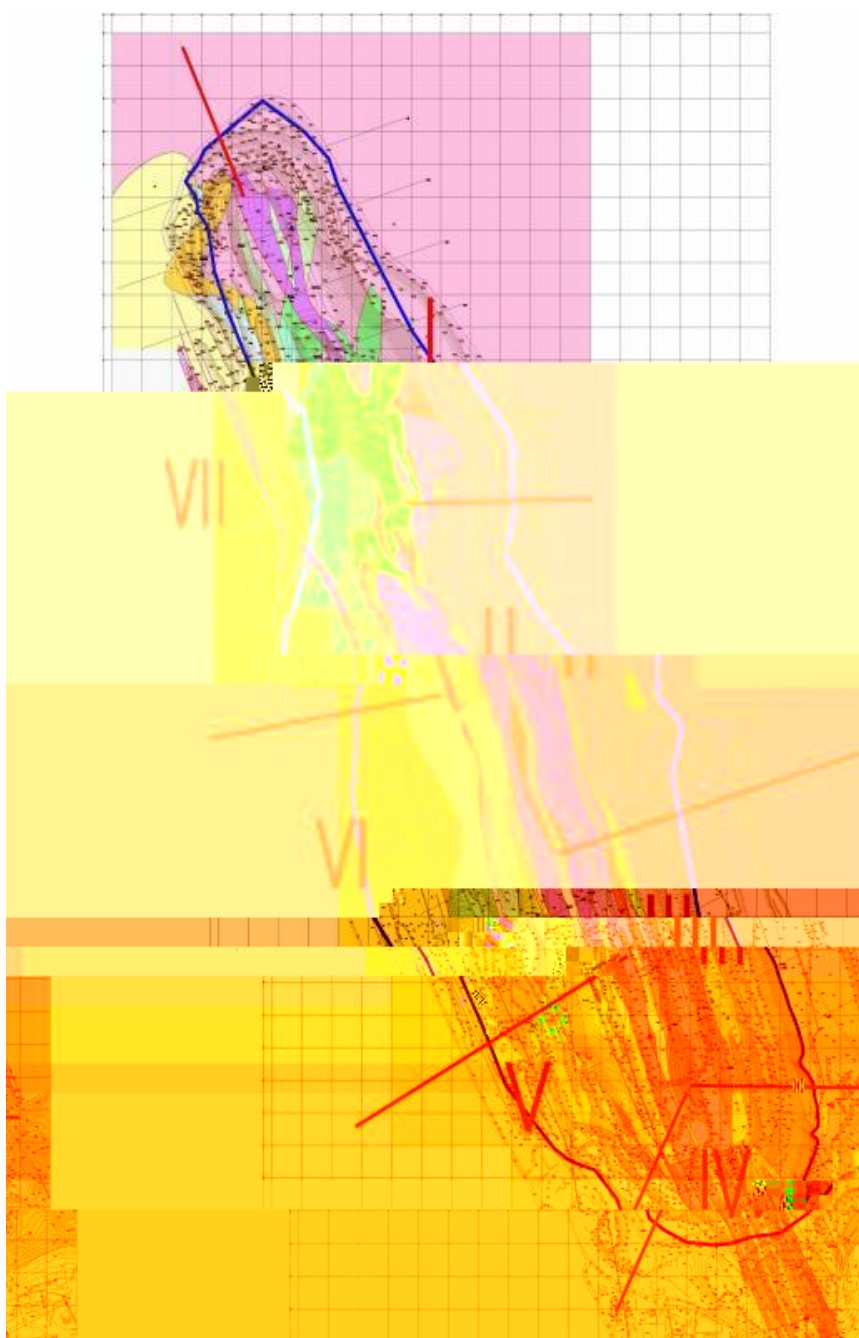
3-11

1.

2.

2023 6





Spencer

Bishop Janbu

c F c

2

596m

Fs=1.25 Fs=1.23 Fs=1.20 I +
II + III + +
Fs 1.25 Fs
1.23 Fs 1.20
3

1 15 1-1' 2-2' 3-3'
4-4' 5-5' 6-6' 7-7' 8-8' 9-9' 10-10'
11-11' 12-12' 13-13' 14-14' 15-15' A-A'
3-6 A-A'
3-7

1994 Hoek GSI RMR Hoek-Brown

$$\sigma_1 = \sigma_3 + \sigma_{ci} \left(m_b \frac{\sigma_3}{\sigma_{ci}} + S \right)^a$$

2002 Hoek 94

D

Hoek-Brown

S a

GSI=25

mb S a

$$= \quad \cdot \quad \left(\frac{\quad}{\quad} \right)$$

$$= \quad \left(\frac{\quad}{\quad} \right)$$

$$= - + - \left[\left(\frac{\quad}{\quad} \right) - \left(\frac{-20}{3} \right) \right]$$

	kN/m ³		/GPa				/MPa		/°		/MPa	
1	24.00	28.00	8.00	33.30	0.25	0.40	4.00	11.00	30.00	42.00	3.40	4.20
2	24.00	28.00	8.00	33.00	0.25	0.40	4.00	11.00	30.00	42.00	3.40	4.20
3	32.00	35.00	69.00	143.00	0.25	0.40	15.00	28.00	40.00	51.00	9.10	15.30
4	32.00	35.00	68.00	84.00	0.25	0.40	11.00	24.00	39.00	45.00	8.30	13.60
5	32.00	35.00	61.00	74.00	0.25	0.40	9.00	23.00	38.00	42.00	6.90	11.80
6	24.00	28.00	25.00	38.00	0.20	0.40	5.00	14.00	35.00	47.00	4.40	10.70
7	24.00	28.00	16.00	31.00	0.20	0.40	8.00	17.00	32.00	38.00	4.70	9.20
8	28.00	31.00	34.00	69.00	.M U							

/					
		Bishop	Janbu	M-P	
1-1'-	1	1.35	1.3373	1.3306	1.3301
1-1'-	2	1.29	1.2831	1.2765	1.2760
1-1'-	3	1.24	1.2534	1.2453	1.2546
2-2'-	1	1.35	1.3328	1.3270	1.3268
2-2'-	2	1.29	1.2793	1.2740	1.2735
2-2'-	3	1.24	1.2436	1.2475	1.2485
3-3'-	1	1.36	1.3494	1.3447	1.3441
3-3'-	2	1.29	1.2806	1.2761	1.2758
3-3'-	3	1.25	1.2554	1.2585	1.25784
4-4'-	1	1.38	1.3557	1.3519	1.3519
4-4'-	2	1.32	1.2963	1.2939	1.2934
4-4'-	3	1.26	1.2678	1.2637	1.2696
5-5'-	1	1.37	1.3462	1.3425	1.3420
5-5'-	2	1.31	1.2913	1.2881	1.2874
5-5'-	3	1.27	1.2731	1.2737	1.2796
6-6'-	1	1.37	1.3515	1.3445	1.3440
6-6'-	2	1.30	1.2880	1.2812	1.2808
6-6'-	3	1.25	1.2567	1.2534	1.2512
7-7'-	1	1.39	1.3767	1.3750	1.3748
7-7'-	2	1.32	1.3101	1.3086	1.3082
7-7'-	3	1.26	1.2675	1.2685	1.2634
8-8'-	1	1.42	1.4078	1.4007	1.4006
8-8'-	2	1.34	1.3344	1.3247	1.3246

/			Bishop	Janbu	M-P
8-8'-	3	1.29	1.2944	1.2946	1.2935
9-9'-	1	1.43	1.4133	1.4066	1.4055
9-9'-	2	1.35	1.3268	1.3246	1.3240
9-9'-	3	1.28	1.2867	1.2858	1.2896
10-10'-	1	1.40	1.3805	1.3763	1.3744
10-10'-	2	1.33	1.3123	1.3086	1.3078
10-10'-	3	1.27	1.2788	1.2785	1.2795
11-11'-	1	1.38	1.3576	1.3503	1.3498
11-11'-	2	1.31	1.2952	1.2885	1.2880
11-11					

J'

042935

GB 51016-2014

3

1

-12m

2

2023 6

3

GB51016-2014



i 'ñ0 ••À
3.5

1/4 @ 1/4 D, €

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6

3.3.2.1

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3

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3

3

1

1

2

3

2

“ ” “ ” “ ”

3.3.2.2

1

3-17

	1. 2. 3.	1. 2.		1. 2.
	1. 2.			1. 2.
	1. 2. 3. 4. 5. 6. 7. 8	1. 2. 3.		1. 2. 3. 4. 5. 6. 7

2

3.3.3.1

1

1

2

3

4

2

1

2

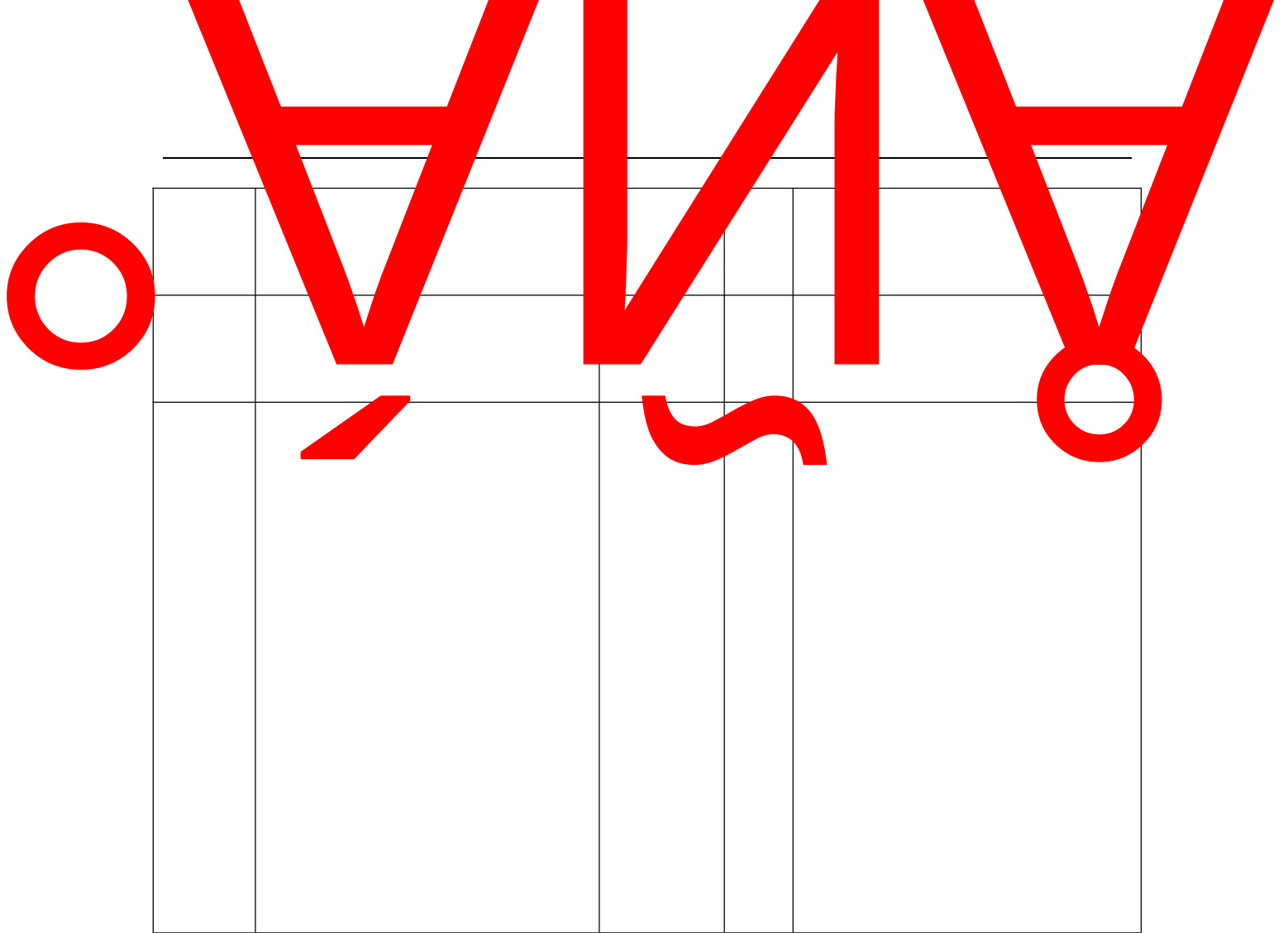
3

3

“ ” “ ” “ ”

3.3.3.2

3-18



3.3.3.3

- 1
- 2
- 3
- 4
- 5
- 6

- 1
- 2
- 3
- 4

“ ” “ ”

3-19

1

2

1

3-20

				90m	66m	42m	
3740.0m	90m		1334m	66m		1048m	42m
966m		350m			C20		2.0m
2.0m		0.30m			0.15m		C30

8

4

2023

 Q_1

Q

50830-2013

20

P=5%

$$Q_2 = F \cdot H \cdot \Phi$$

$$Q_2 = F \cdot H_p \cdot \Phi$$

$$Q_2 = \text{m}^3/\text{d}$$

$$Q_2 = \text{m}^3/\text{d}$$

$$F = \text{m}^2$$

$$H = \text{m}/\text{d}$$

$$H_p = P=5\% \quad \text{m}/\text{d}$$

$$\Phi =$$

5237145m²

35.2mm

24h 48h 72h 120h 168h

P=5%

h	P=5% mm
24	189.00
48	209.42
72	252.00
120	275.67
168	304.95

		F m ²	H m/d	φ	Q ₂ m ³ /d	
		5237145	0.0352	0.4	73739	
	24h	5237145	0.189	0.6	593892	P=5%
	48h	5237145	0.20942	0.6	658058	P=5%

$$H_{-120\text{m}} = 1.15 \times (162 + 5) = 192.1\text{m} \qquad +42\text{m}$$

3-25

“ ”

5.

1.

2.

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4.

1.

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4.

		320m 15553 m ³ -300m 30m 330m 30m 36~37 30m 22.57	
2.	5.5		
3.	5.6		

3.6.3.1

2020 10

2022 2

280m

320m

1

Spencer Bishop Janbu

c φ F

c' φ'

2

GB51119-2015

3-28

3-28

		H m	V 10 ⁴ m ³
		H 180	V 20000
		120 H≤180	5000 V≤20000
		60 H≤120	1000 V≤5000
		H≤60	V≤1000

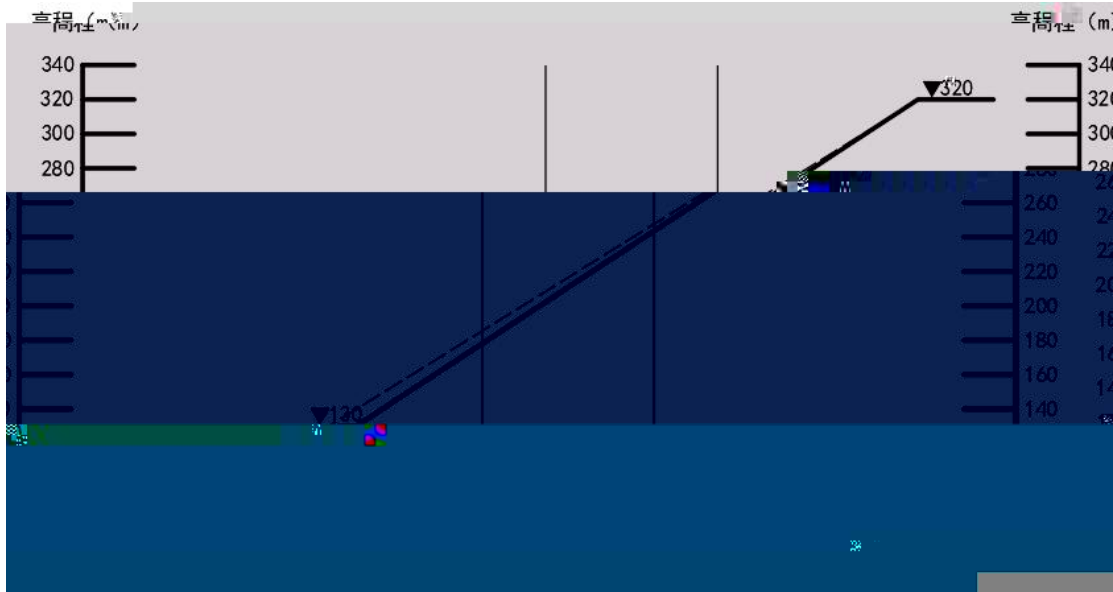
GB51119-2015

3-29

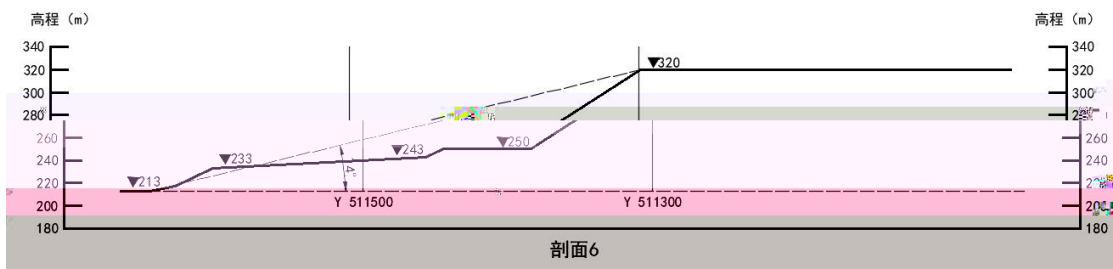
1.25

3-29

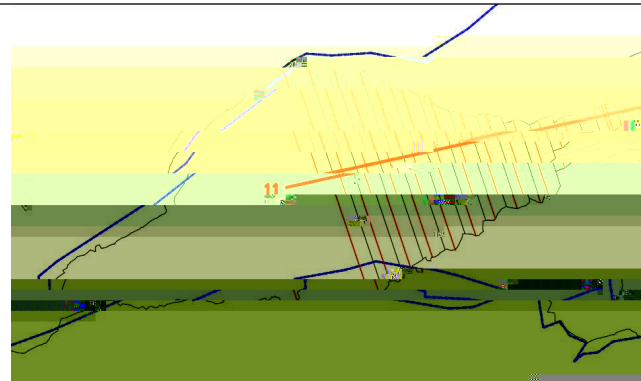
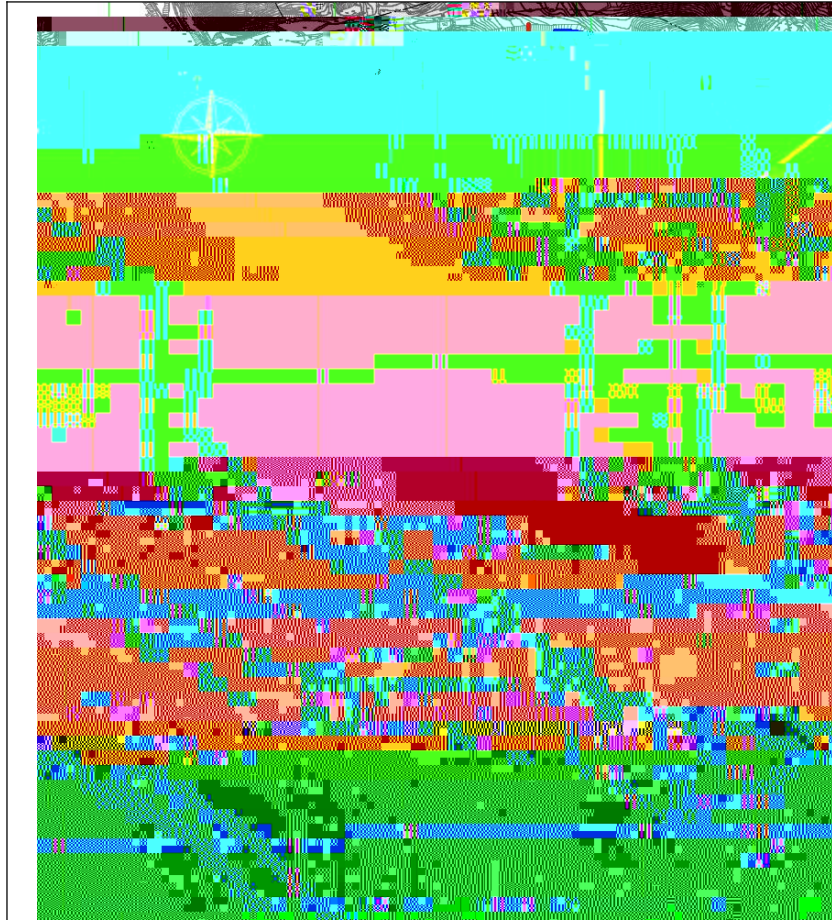
	1.25 1.30
	1.20 1.25
	1.15 1.20
	1.10 1.20



3-8 2-2



3-9 6-6



3-10

4

Hoek-Brown

3-30

	3-30									
	/	kN/m ³	kN/m ²	°	°	10 ⁴ MPa		10 ⁴ MPa	10 ⁴ MPa	MPa
1		21	5	34	4	1.2	0.2	0.667	0.500	0.01
2		19.5	33	16	0	0.004	0.31	0.004	0.002	0.15
3		19.5	30	16	0	0.004	0.31	0.004	0.002	0.15
4		19.5	8	26	0	0.23	0.25	0.135	0.150	

5 0-0,-	1	I'30	I'34I0	I'3302	I'3304
8-8,-	3	I'53	I'53I4	I'5325	I'5325
8-8,-	5	I'50	I'54ΔI	I'544I	I'5445
8-8,- 3-31	1	I'32	I'3323	I'3352	I'3350
Δ-Δ,-	3	I'54	I'540Δ	I'545I	I'540I
Δ-Δ,-	3-31 5	I'58	I'5080	I'5023	I'5022
Δ-Δ,- /	1	I'32	I'334I Bishop	I'3303 Janbu	I'3302 M-P
0-0,-	3	I'50	I'5082	I'5032	I'5005
1-1'-	1	1.35	1.3299	1.3269	1.3270
0-0,-	5	I'35	I'3008	I'50ΔΔ	I'50Δ0
1-1'-	2	1.28	1.2648	1.2617	1.2618
0-0,-	1	I'4I	I'3802	I'3833	I'383I
1-1'-	3	1.25	1.2467	1.2486	1.2478
2-2,-	3	I'50	I'520Δ	I'52Δ8	I'5230
2-2'-	1	1.34	1.3248	1.3216	1.3217
2-2'-	2	1.28	1.2593	1.2561	1.2562
2-2'-	3	1.24	1.2467	1.2424	1.2413
3-3'-	1	1.36	1.3370	1.3337	1.3338
3-3'-	2	1.29	1.2715	1.2684	1.2684
3-3'-	3	1.25	1.2546	1.2574	1.2574
4-4'-	1	1.34	1.3143	1.3107	1.3108
4-4'-	2	1.27	1.2493	1.2458	1.2459
4-4'-	3	1.23	1.2355	1.2352	1.2371
5-5'-	1	1.40	1.3853	1.3817	1.3818
5-5'-	2	1.31	1.2918	1.2884	1.2885

/						
			Bishop	Janbu	M-P	
9-9'-	2	1.30	1.2770	1.2747	1.2745	
9-9'-	3	1.24	1.2464	1.2463	1.2425	
10-10'-	1	1.35	1.3256	1.3221	1.3220	
10-10'-	2	1.28	1.2622	1.2589	1.2587	
10-10'-	3	1.24	1.2412	1.2462	1.2424	
11-11'-	1	1.43	1.4120	1.4093	1.4092	
11-11'-	2	1.34	1.3273	1.3247	1.3247	
11-11'-	3	1.27	1.2747	1.2746	1.2790	

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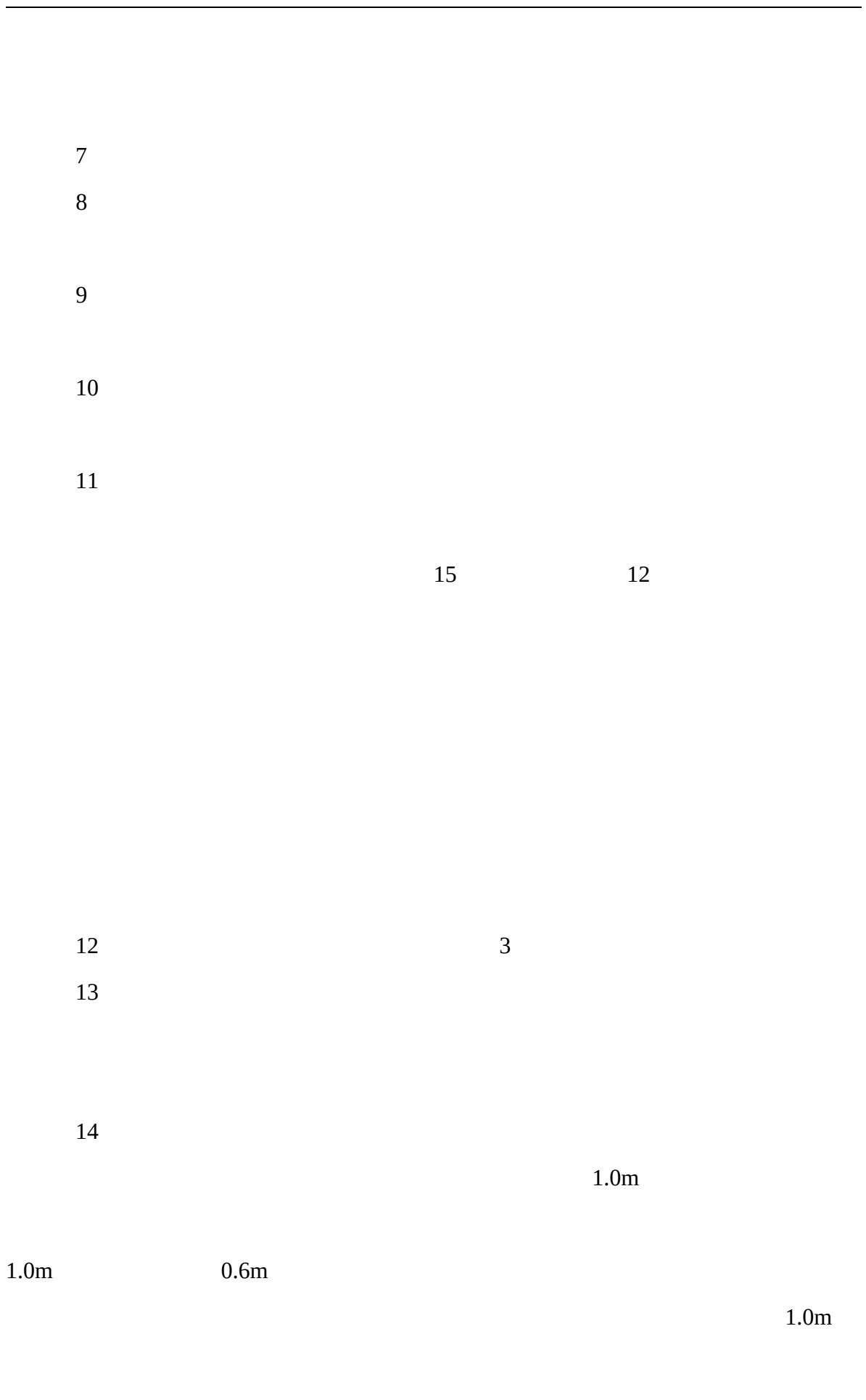
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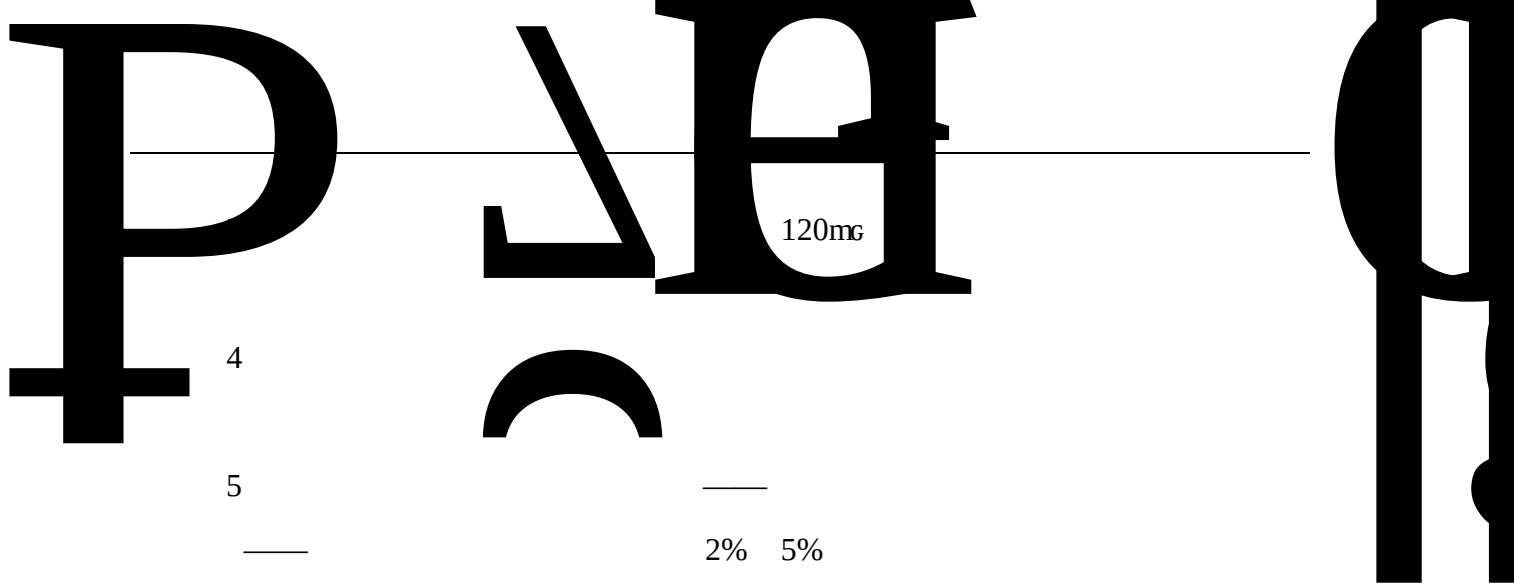
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$$2 \quad \text{m} \begin{array}{c} \parallel \\ \parallel \\ \parallel \end{array} \begin{array}{c} \text{H}' \\ \text{F} \end{array}$$

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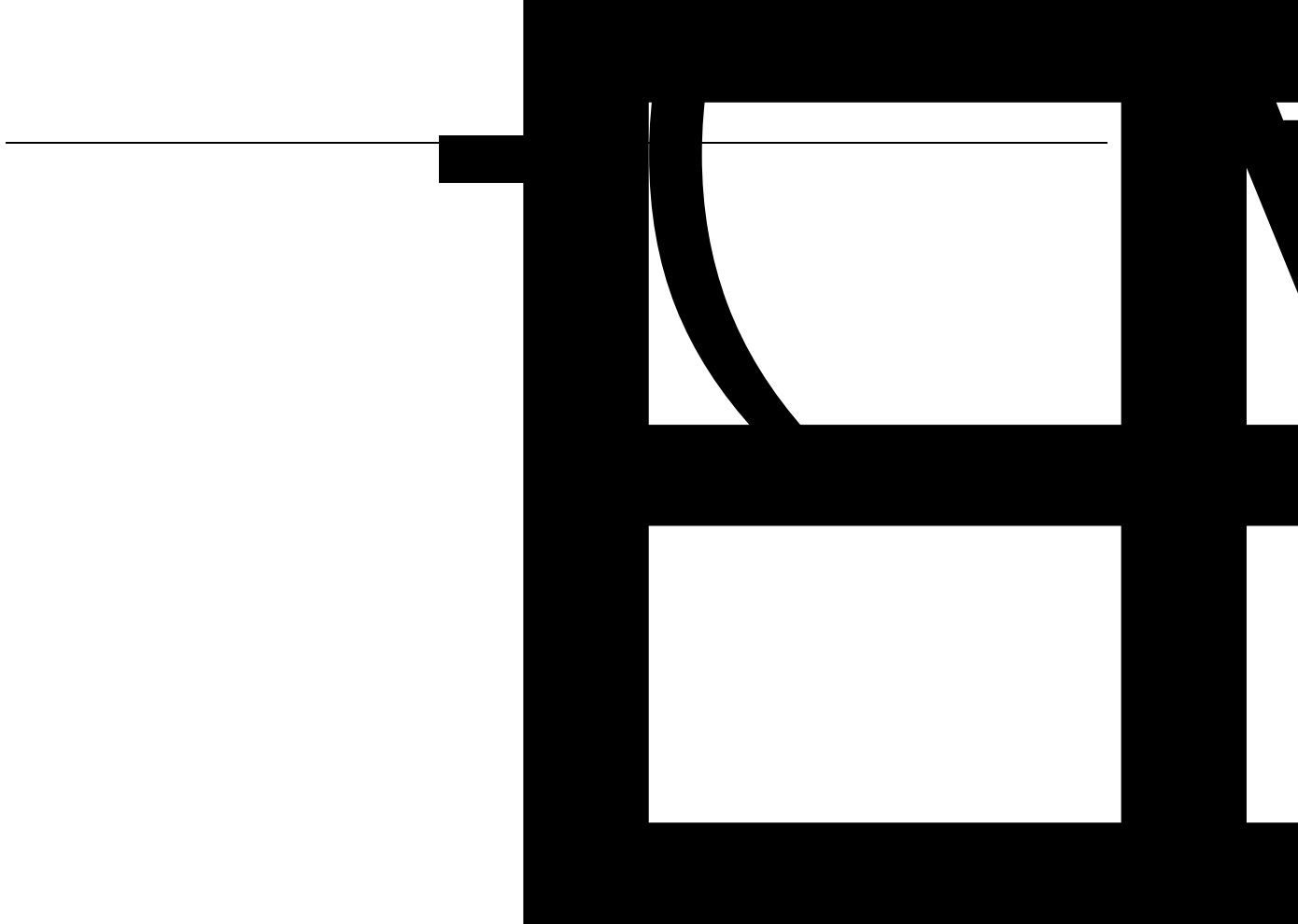
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3 42m

4 -120m

5 -300m

6 -450m

7 3250

8 3850

